TFAWS Passive Thermal Paper Session



High Temperature Water-Titanium Heat Pipe Radiators for the Kilopower Fission Power System



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Outline



- Motivation
- Objectives
- Evaporator Design, Fabrication, and Testing
- Radiator Trade Study
- S-Bonded Radiator Fabrication and Testing
- Key Results & Future Work
- Acknowledgements

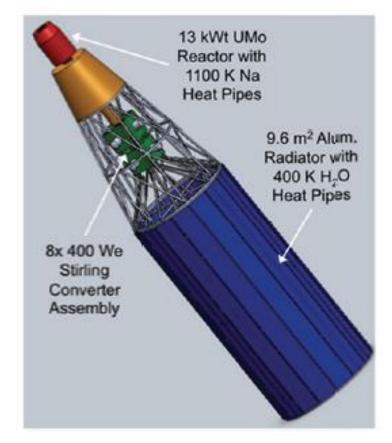




Motivation



- NASA Glenn is examining small fission reactors for future space transportation and surface power applications
 - These Kilopower reactors would have an 8 to 15 year design life that could be available for a 2020 launch to support future NASA science missions
 - Both 1 kWe thermoelectric and 3 kWe
 Stirling systems have been examined
- Titanium-Water heat pipes have been proposed to transport the waste heat from the Stirling converters to the system radiator



Mason, Gibson, and Poston, 2013





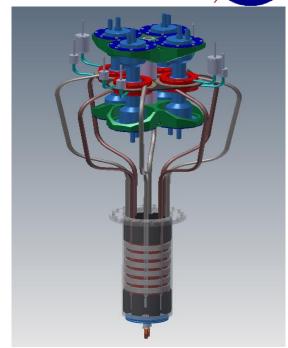
Objectives – (Phase II SBIR)

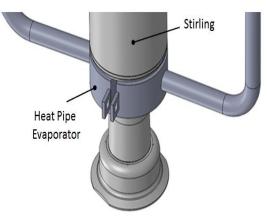
NASA

- Overall objective: develop full-length titanium water heat pipes for testing with the Stirling convertors on the Kilopower demonstration unit
 - Four Heat pipes/Two Stirling convertors

Sub-objectives:

- Design the heat pipe evaporator to interface with the cold end of the Stirling convertor
- Design the radiator
- Extensive freeze/thaw testing
- Fabricate 4 heat pipes with radiator fins
- Testing of heat pipes at ACT, followed by NASA Glenn
- Design of prototypic ISS experiment
- Additional heat pipe for shock and vibration tests





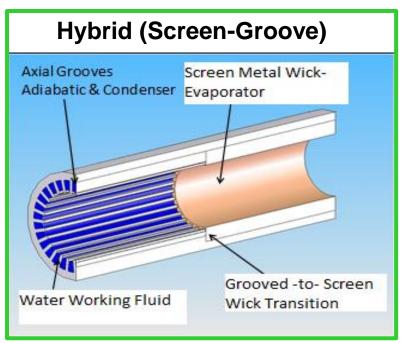


Heat Pipe Wick

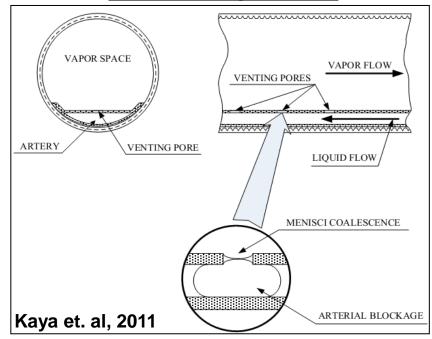


- Wick must accommodate four operating conditions:
 - Space: Zero gravity; capillary forces must drive liquid return to evaporator
 - ◆ Earth, Slightly adverse: 0.1" 0.3" evaporator superior to condenser
 - <u>Earth, Gravity Aided</u>: Fluid returned to evap. by gravity (thermosiphon)
 - <u>Launch</u>: Evaporator is superior to condenser; wick deprimes

Suitable Wick Structures



Self-Venting Arterial





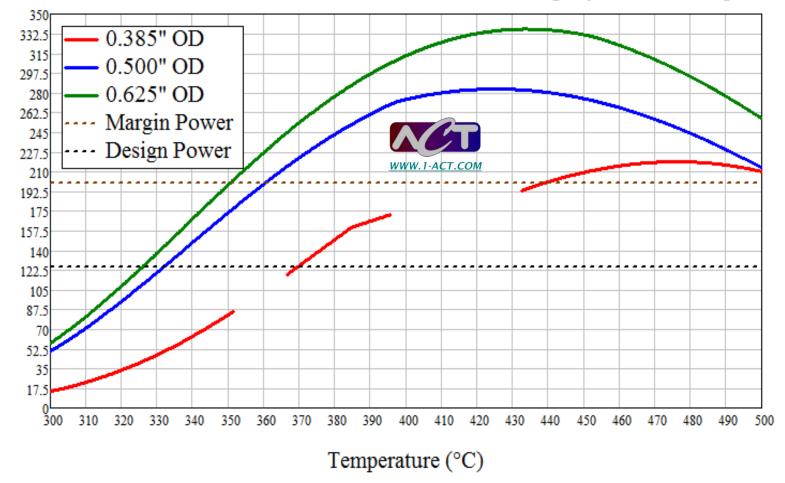


Power (W)

Predicted Heat Pipe Performance



Performance Predictions for a xin OD, 67" Long Hybrid Heat Pipe



0.5" outer diameter hybrid (screen-groove) heat pipe was selected

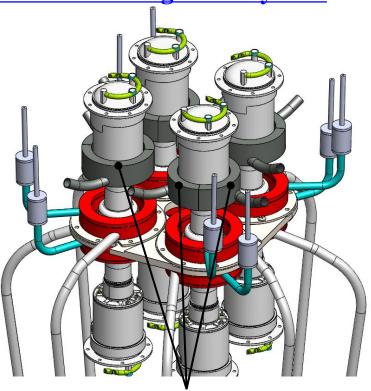




Evaporator Design

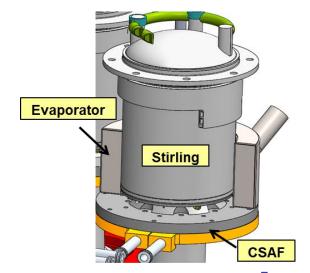


View of Stirling engines and thermal management system



(Stirling cold end heat pipe evaporators colored dark grey)

- The cold end of the Stirling engine is connected to the radiator panels via titanium water heat pipes
 - In order to prevent damage from freezing of the working fluid in the heat pipe grooves, an accumulator will be used to contain the fluid
 - ➤ The heat pipes will mount to CSAF instead of directly to the Stirling
 - Additionally, the heat pipes will be tested with a annular heater block (inner diameter surface of evaporator)







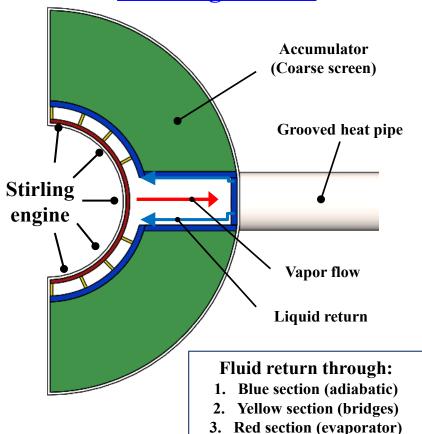
Bi-porous Wick Design (Evaporator)



Dynamics of working fluid

- $r_{c_{fine_screen}} < r_{c_{coarse_screen}} < r_{c_{grooves}}$
- At the interface of the grooved heat pipe and evaporator, only the fine screen is in contact with the grooves.
- This ensures that coarse screen (accumulator) fills with fluid only when the fine screen is saturated and there is no heat applied to the evaporator.
- Therefore the accumulator only fills with fluid when the heat pipe is not in operation

Common fluid return for all configurations





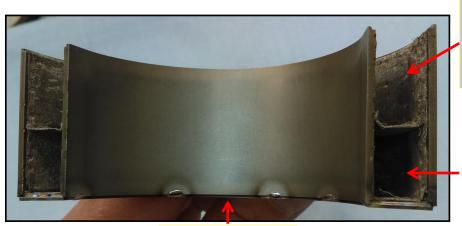
(Note: all are of fine screen)



Evaporator Fabrication (CSAF)

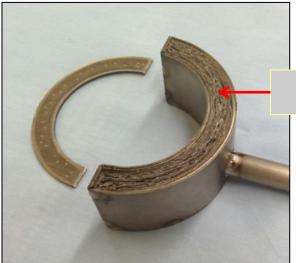


The evaporator is a weldment where each piece is screened individually



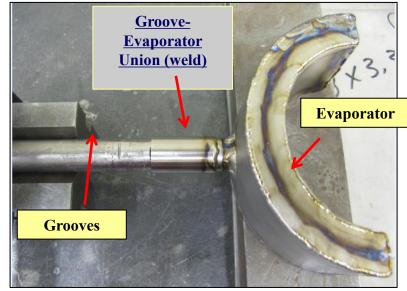
Accumulator
To be filled with
100 size mesh

Vapor Space
Lined with 150
size mesh



Heat Input Surface

Accumulator







Evaporator

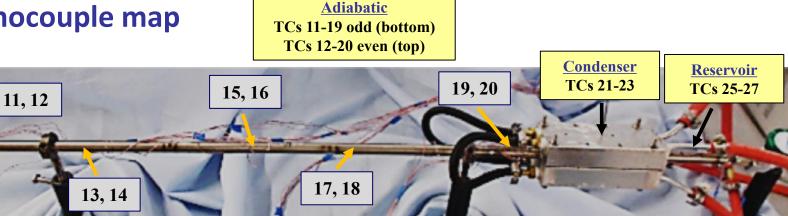
TCs 1,2,8

Accumulator TCs 5,6

Evaporator Testing



Thermocouple map



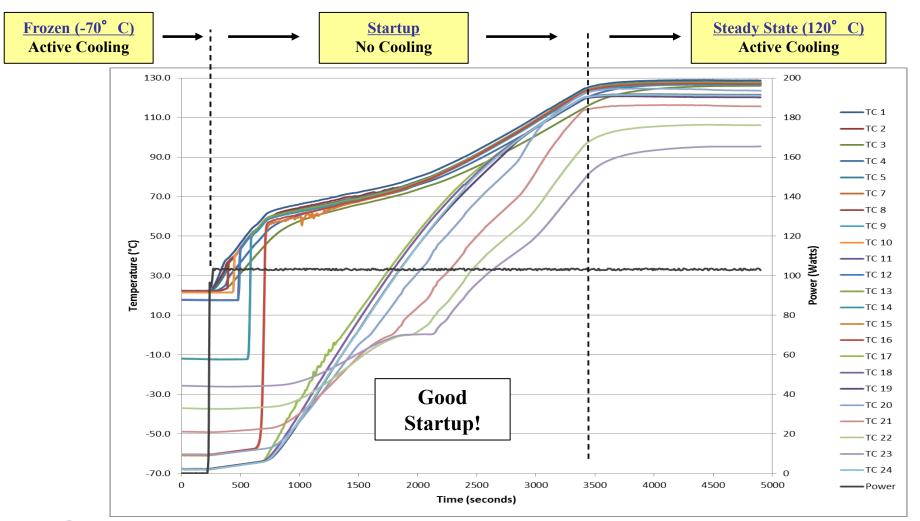
Test details

- Grooved heat pipe (from Phase I) length: 34" (reservoir, condenser, adiabatic)
- Condenser length: 5"
- NCG Reservoir length: 3"
- Heater block only applies heat to the evaporator (not the accumulator)
- Accumulator is inferior to the evaporator for all test cases



Freeze-Thaw Startup Test

- NASA
- The condenser was cooled to -70° C and a step input of 100 Watts was applied
- Active cooling was suspended until heat pipe reached operating temp. of 120° C



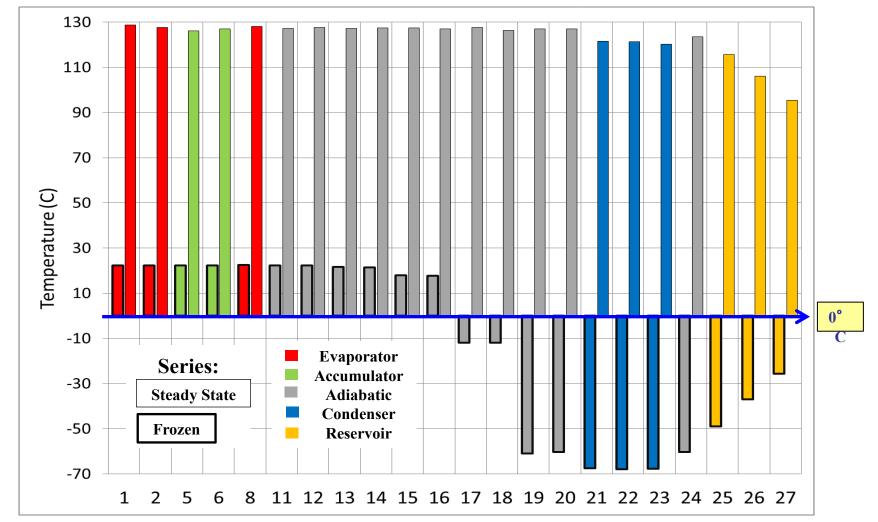




Freeze-Thaw Startup Test



Snapshot of temperature distribution at frozen and steady state



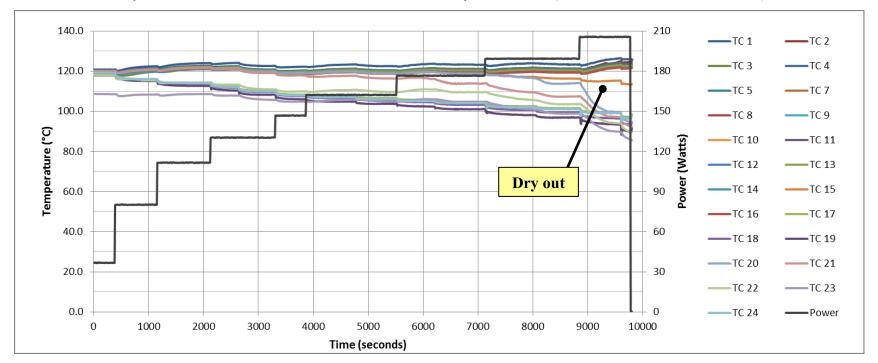




Performance Testing



- Initial performance tests showed ~130 Watt transport
 - Does not meet requirement (250 Watt)
 - Monel screen was used in place of Titanium because of cost, but was not oxidized for proper wetting; therefore we suspect wetting angle is large, so capillary pumping is small
 - Performed a non-invasive oxidation procedure to treat the Monel screen
- Performance test after oxidation showed 190 Watt transport
 - Improvement, but still does not meet requirement (oxidation not sufficient)

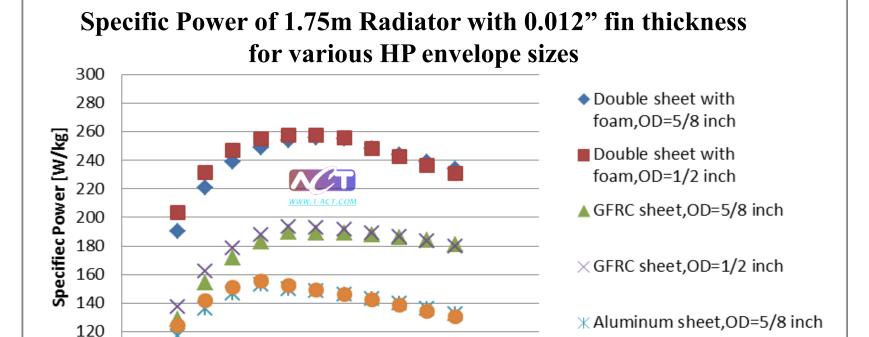






Radiator Trade Study: Specific Power





• The \uparrow W/kg, the \uparrow $q_{transport}$ and \downarrow mass

5

Fin width [inch]

Optimal fin width: ~6 inches

100

0



10

15

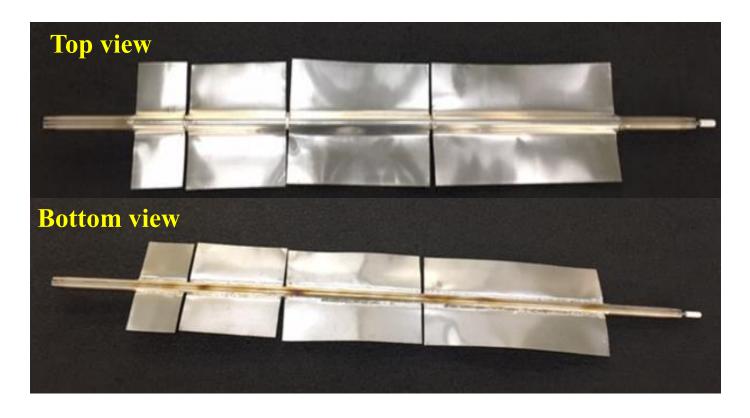
Aluminum sheet,OD=1/2 inch



Aluminum Radiator



- Aluminum radiator is cheaper and more readily available than GFRC or double sheet with honeycomb panels and POCOFoam saddles
- S-Bond is a high temperature solder for Aluminum to Titanium
- Prototype thermosyphon radiator

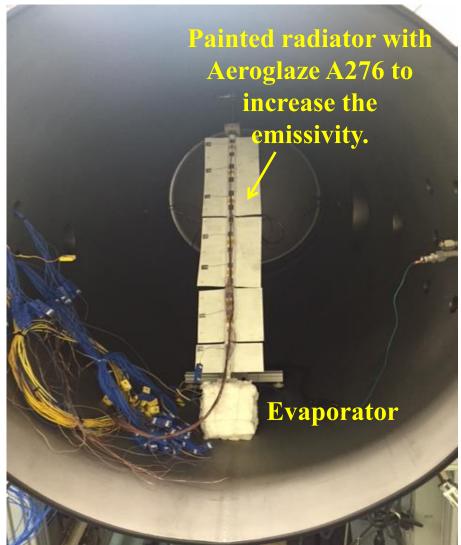


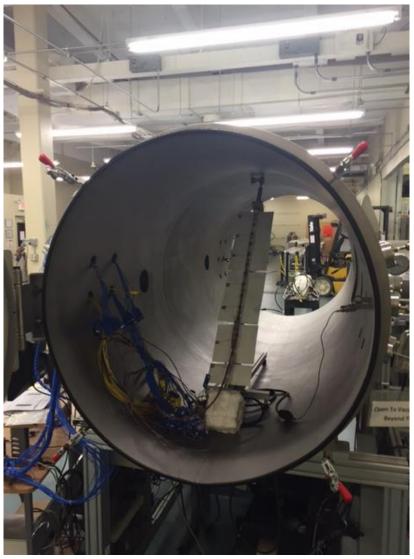




Testing in the Vacuum Chamber





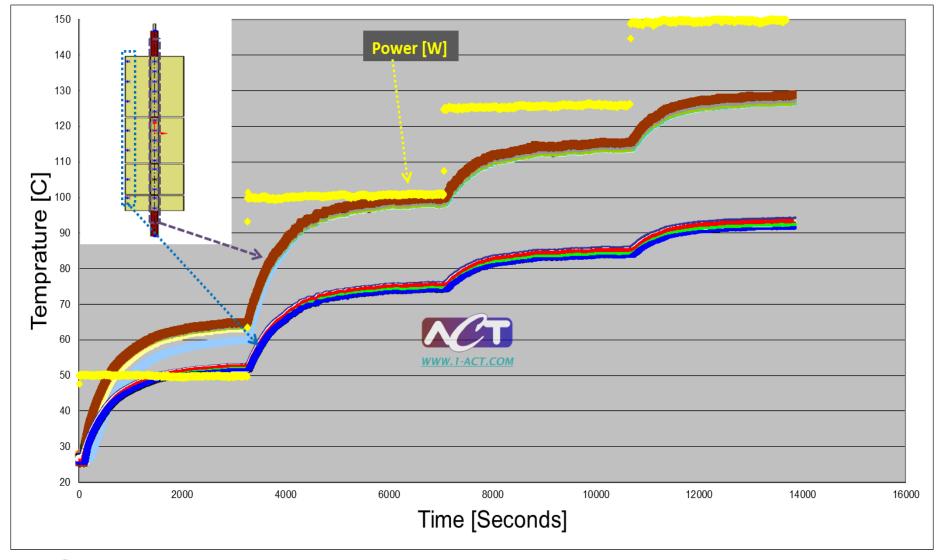






S-Bonded Radiator Performance Test: Vacuum



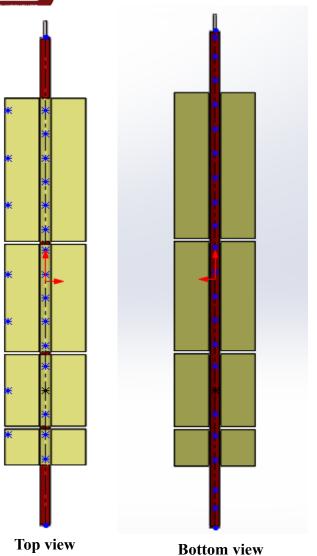






Results in Vacuum





Fin	Titanium	Aluminum
	13 126.72	
	12 126.85	
	11 126.76	
36 91.44	10 127.73	128.65 29
		128.52 28
35 92.40	9 128.01	128.06 27
24 02 04	0 400 44	128.06 26
34 93.01	8 128.14	128.67 25 127.69 24
		127.69 24 127.91 23
33 92.81	7 126.99	128.03 22
33 32.01	7 120.33	128.14 21
32 92.17	6 126.77	128.16 20
02 02.11	0 120111	126.87 19
		126.20 18
31 93.50	5 127.66	127.70 17
		127.92 16
		127.40 15
30 93.13	4 127.63	127.41 14
	3 127.08	
	2 132.50	
	1 134.75	
Anni	lied Power Watts 150.51	





Testing in Ambient with Painted Radiators

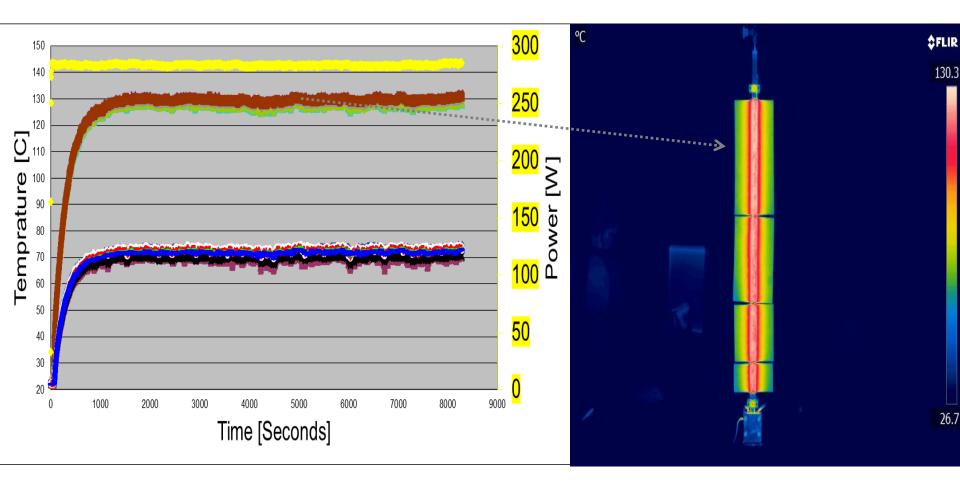






Results – Thermal Imaging in Ambient



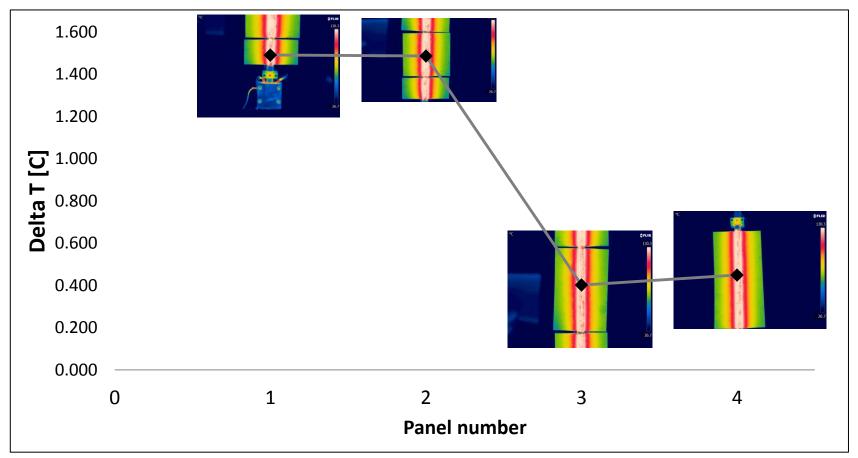






△Temperature heat pipe and root of aluminum fin







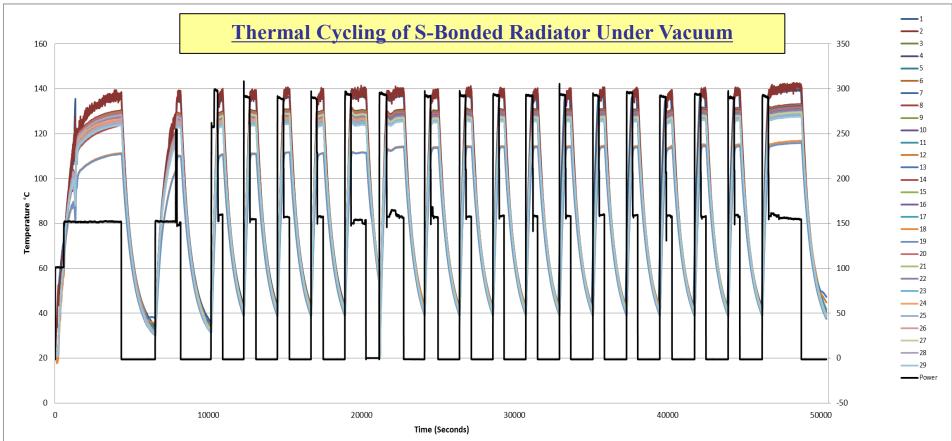


Radiator Thermal Cycle Testing



Tested S-Bond for viability titanium - aluminum joint

- Preliminary testing shows positive results
 - Low temperature gradient (0.3 C) across joint
 - 19 cycles in vacuum environment from 40 C to 140 C without degradation





Key Results & Future Work



Key Results

- Developed a working hybrid heat pipe with similar geometry to final configuration
- Demonstrated freeze-thaw capability of hybrid heat pipe
- Developed Aluminum radiator using S-Bond
- Validated radiator performance by testing in vacuum and ambient

Future Work

- Revise evaporator design for better performance
- Integrate heat pipe and radiator thermal models to determine final configuration
- Fabricate and test 4 heat pipe radiator deliverables





Acknowledgements



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- We would like to thank Maxwell Briggs and Marc Gibson for their helpful suggestions





Questions?







